

Kelland Homes

Zoning Submission Regarding Lands at Newtown Little & Newtownpark, Blessington, Co. Kildare

Flood Risk

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REVISION HISTORY

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Project	Zoning Submission Regarding Lands at Newtown Little & Newtownpark, Blessington, Co. Kildare
Title	Flood Risk

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1. INTRODUCTION

Kelland Homes Ltd. ['the Applicant'] is seeking an amendment to the draft Kildare County Development Plan 2023 – 2029 comprising the re-classification of lands ['the Site'] at Newtown Little & Newtownpark, Blessington, Co. Kildare.

The extent of the Site and the streams located in or close to it are shown on Figure 1-1.

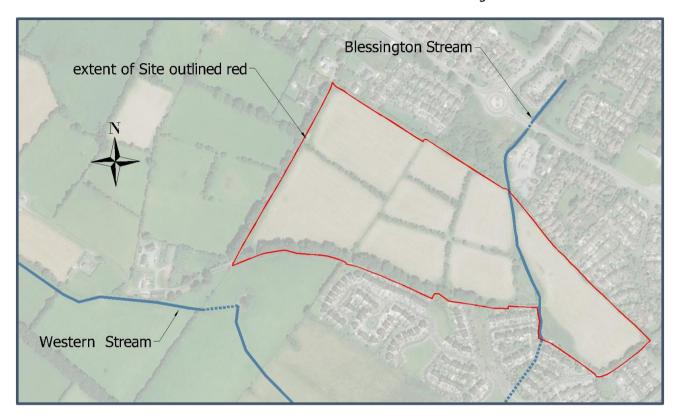


Figure 1-1 Site Location and Context

Figure 1-2 is reproduced from the draft County Development Plan and shows the land-use classification proposed at the Site. This proposed classification differs from the current development plan in that:

- an area of land, corresponding to a flow path for fluvial overland flow through the Site during extreme events, has been re-classified from New Residential to Amenity;
- all lands within the Site located east of the Blessington Stream and a corridor adjacent to the western boundary of the Blessington Stream have been re-classified from New Residential to Amenity;

This proposed classification severs the western part of the Site. This report proposes an alternative route for overland flow through the Site which would allow this severance to be eliminated (Sections 2 and 3 refer).

This proposed classification eliminates development in the eastern side of the Site. This report demonstrates that the eastern part of the Site can be developed in compliance with the Flood Risk Management Guidelines. (Section 4 refers).

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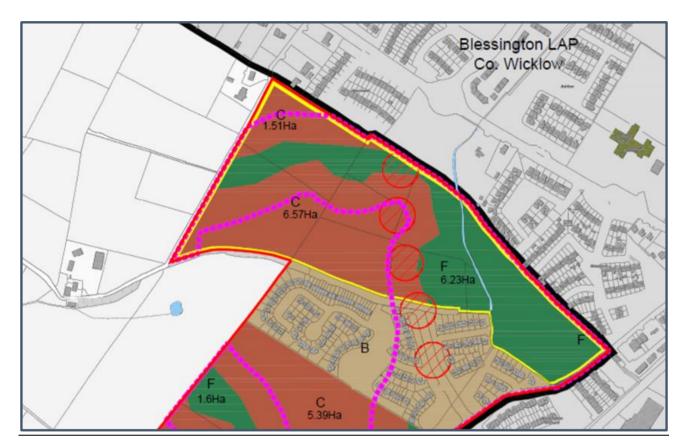


Figure 1-2 Proposed Land-Use Classification

2. FLOOD RISK AT THE SITE ARISING FROM OVERLAND FLOW

CFRAM maps prepared for the CFRAM study programme flood risk from overland flow. The source of this overland flow is a watercourse ['the Western Stream'] which flows in a southerly direction to the west of the Site. The mapping suggests that during extreme rainfall events, the hydraulic capacity of the watercourse will be exceeded, and the exceedance water will flow overland to the western boundary of the Site. This overland flow pattern is similar to and consistent with the flood risk identified in the SFRA prepared for the draft County Development Plan 2023 – 2029. A copy of the relevant CFRAM flood risk map is provided in Appendix A.

Figure 2-1 shows the route for this overland flow through the Site.

The Western Stream is culverted at a point approximately 100m west of the Development Site. The culvert comprises a 450mm dia. pipe and is of lower hydraulic capacity than the channel / ponds upstream and downstream of it. This lower hydraulic capacity is the primary cause the overland flow which occurs upstream of the culvert.

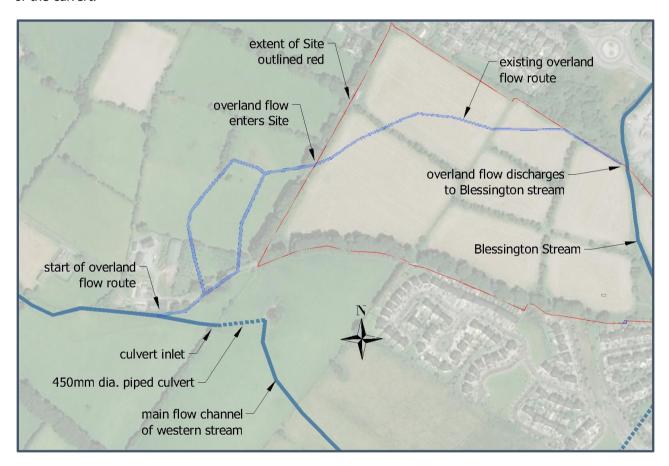


Figure 2-1 Overland Flow Route

3. ALTERNATIVE ROUTE FOR OVERLAND FLOW

3.1. Calculation of overland flow rate

The catchment for the Western Stream is shown in Figure 3-1 and measures 0.76km².

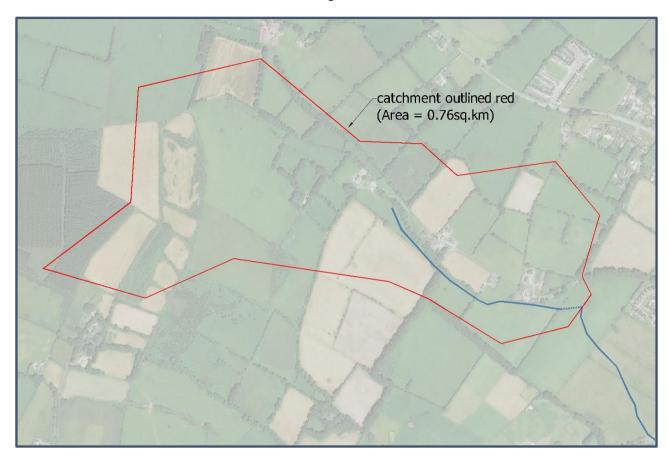


Figure 3-1 Catchment of Watercourse west of Site

The OPW Web Portal advises particular caution where peak flows are being estimated for catchments of less than 25km^2 . Accordingly, peak flows in the watercourse are estimated using IH124 (Flood Estimation for Small Catchments). Details of these calculations are included in Appendix B and the results summarised in Table 3-1. These estimates include a climate change factor of +20%. Table 3-1 also shows the equivalent peak flood flows as predicted by CFRAM. The CFRAM flows are higher and so, applying the precautionary principles, these higher flows are used for this assessment.

Return Period	Symbol	IH124 (m³/s)	CFRAM (m³/s)s
Mean Annual Average	Q _{bar}	0.32	
100 years (1% AEP)	Q100	1.04	1.36
1000 years (0.1% AEP)	Q ₁₀₀₀	1.38	2.40

Table 3-1 Peak Overland Flow (after applying 20% Climate Change Factor)

The piped culvert that restricts the capacity of the watercourse is 450mm dia. Based on the following conservative assumptions, the rate of overland flow through the Site is estimated to be 2.0m³/s.

- the headwater at the culvert inlet cannot exceed 1.0m, the culvert has a capacity of 0.4m³/s;
- during a 0.1% AEP event, all flow exceeding the capacity of the culvert becomes overland flow to the Development Site.

3.2. Alternative Route for Overland Flow

Figure 3-2 shows an alternative route for the overland flow risk at the Site. This alternative route is created by forming an open channel to the north of the existing route which has the capacity to carry the overland flow rate associated with the 0.1% AEP event.

Details of the alternative overland flow route are provided in Appendix C.

The alternative route is selected to be as close to the northern boundary of the Site as possible and thus minimise the severance caused by the need to accommodate this overland flow risk.

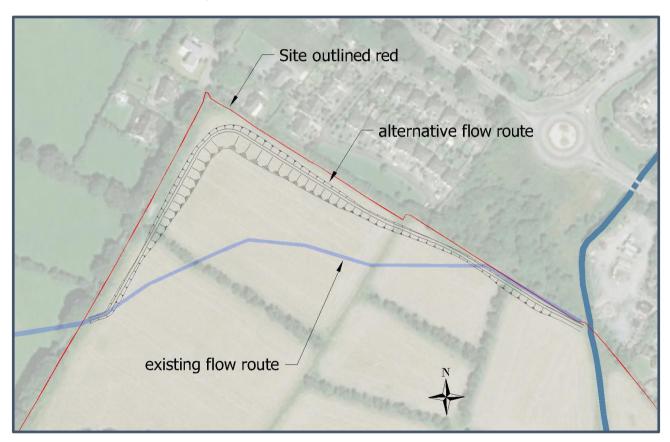


Figure 3-2 Alternative Route for Overland Flow

4. DEVELOPMENT OF THE EASTERN SIDE OF THE SITE

A preliminary design for development of the Site was prepared in 2003 [referred to hereafter as 'the Development']. As part of the design process, an initial assessment of flood risk was carried out in accordance with the Flood Risk Management Guidelines. This initial assessment identified indicators of fluvial flood risk at the Site and so detailed assessment of fluvial flood was carried out.

4.1 Estimating Peak Flood Flows

The catchment area for the stream, shown on Figure 4-1, measures 6.48 km².

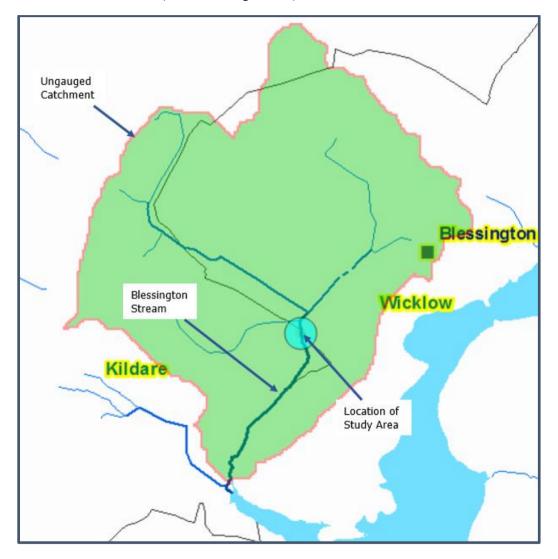


Figure 4-1 Catchment Area for Stream

The OPW provides a Web Portal for estimating peak flood flows in natural catchments (Flood Studies Update (FSU) Web Portal). While the use of this Portal is generally considered best practice for the estimation of flood flows, the Portal advises particular caution where peak flows are being estimated for catchments of less than 25km². Accordingly, peak flows in the stream are estimated using IH124 (Flood Estimation for Small Catchments). Details of these calculations are included in Appendix D and the results summarised in Table 4-1. These estimates include a climate change factor of +20%.

Table 4-1 also shows the equivalent peak flood flows as predicted by CFRAM. The CFRAM flows are slightly higher and so, applying the precautionary principles, these higher flows are used for this assessment.

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Return Period	Symbol	IH124 (m³/s)	CFRAM (m³/s)
Mean Annual Average	Qbar	0.478	
100 years (1% AEP)	Q100	6.99	7.01
1000 years (0.1% AEP)	Q1000	9.28	9.68

Table 4-1 Peak Fluvial Flows (after applying 20% Climate Change Factor)

4.2 Model

A topographical survey was carried out for the study area by a third-party land surveyor. The results of this survey were imported into the industry standard software package Infrastructure Ultimate Design Suite to create a 3D digital terrain model for the study area.

A hydrological model was prepared to simulate flow patterns during the 100 year and 1000 year rainfall events. This model was developed using the River and Flood Analysis module of the industry standard package Infrastructure Ultimate Design Suite produced by Autodesk. The hydrological modelling within this module is itself based on the HEC-RAS modelling software produced by the US Army Corps of Engineers.

The module calculates flood risk zones for the catchment based on the peak flood flows and the following:

- the terrain model;
- cross-sectional data for the river channel;
- dimensions of culverts and other drainage structures;
- appropriate values for the roughness coefficient 'Manning's n' as determined from visual inspection of the Development Site.

The flow volumes in Table 4-1 significantly exceed the capacity of the 1200mm dia. culvert into which the stream discharges at the southern boundary. Surcharged water will overtop the wall at the southern boundary when the surcharged water level reaches 194.80m. The model therefore assumes a downstream water level of 194.80m.

4.3 Existing Fluvial Flood Risk Zones at the Site

Figure 4-2 contains a map showing the existing fluvial flood risk zones determined using the hydrological model described above superimposed on the emerging layout for the Development.. Peak water levels are as follows:

- 1.0% AEP Flood Event 194.80m
- 0.1% AEP Flood Event 194.82m

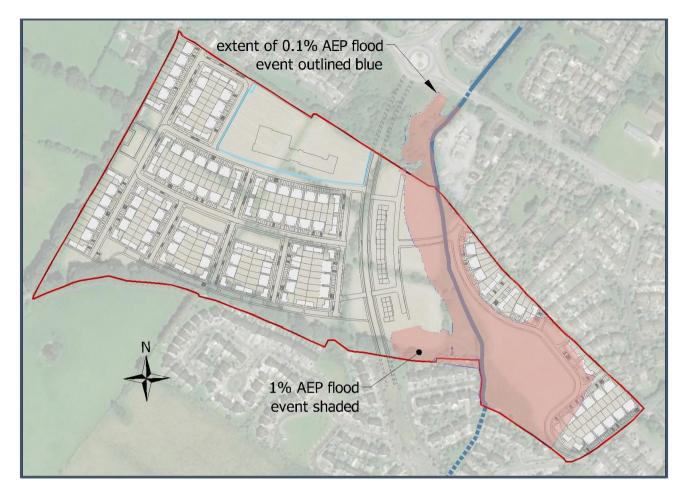


Figure 4-2
Existing Flood Risk Zones Associated with Blessington Stream superimposed on the Development Layout

4.4 Compensatory Storage

While the layout of the Development is broadly cognisant of fluvial flood risk, elements of the proposed development, in particular roads, encroach on the flood risk zones. This creates the potential for the proposed development to displace floodplain storage and thereby increase flood risk elsewhere. To prevent this, it is necessary to provide compensatory storage within the Site. Compensatory storage is provided by reducing the existing ground level immediately adjacent to the stream to create a basin. Figure 4-3 shows the general layout of the two compensatory storage areas that are proposed.

The requirements for providing compensatory storage are set out in the Appendix to the Flood Risk Management Guidelines. Normally it is calculated by comparing volumes taken by the development and the volume offered by the compensatory storage for a number of horizontal slices through the range defined above - the thickness of a slice should be typically 0.1 metres.

The compensatory volume should be at the same level (within reasonable working limits) as the lost storage for each slice. Compensatory storage cannot be located in an area where water-vulnerable development is proposed.

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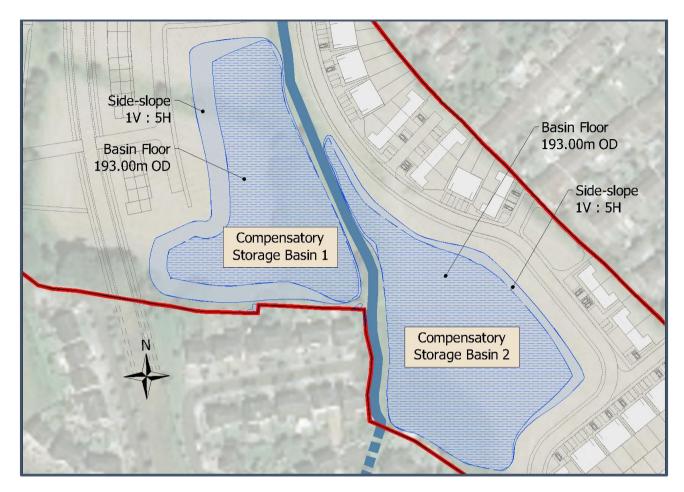


Figure 4-3 Compensatory Storage Basins

The industry standard package Infrastructure Ultimate Design Suite (by Autodesk) was used to create surface models for the existing site and for the finished level of the proposed development. Comparison models were then created using these surfaces.

Table 4-2 presents the results of this modelling and shows that for nearly all elevation intervals, the volume of compensatory storage provided actually exceeds the volume of floodplain storage displaced. There is loss of floodplain at only the highest levels. Cumulatively, significantly more floodplain storage will be available upon completion of the proposed development than is currently available, thereby reducing fluvial flood risk elsewhere.

	Storage	Change in		
Elevation (m OD)	Pre-Development	Post-Development	Storage	
193.00	663	799	136	
193.10	754	1,645	891	
193.20	853	1,703	850	
193.30	956	1,749	793	
193.40	1,060	1,789	729	
193.50	1,164	1,828	664	
193.60	1,277	1,875	598	
193.70	1,426	1,937	511	
193.80	1,562	2,016	454	
193.90	1,703	2,109	406	
194.00	1,821	2,171	350	
194.10	1,931	2,224	293	
194.20	2,041	2,270	229	
194.30	2,164	2,312	148	
194.40	2,309	2,353	44	
194.50	2,489	2,394	-95	
194.60	2,716	2,436	-280	
194.70	2,995	2,490	-505	
194.80	3,277	2,570	-707	
	5,509			

Table 4-2 Available Floodplain Storage: Pre- and Post-Development

4.5 Flood Risk Zones Post-Development

Figure 4-4 shows the flood risk zones associated with the Stream Post-Development. Flood Risk zones are confined to open spaces and do not encroach on water-vulnerable elements of the proposed development. Peak water levels are effectively the same as pre-development:

- 1.0% AEP Flood Event 194.81m
- 0.1% AEP Flood Event 194.82m

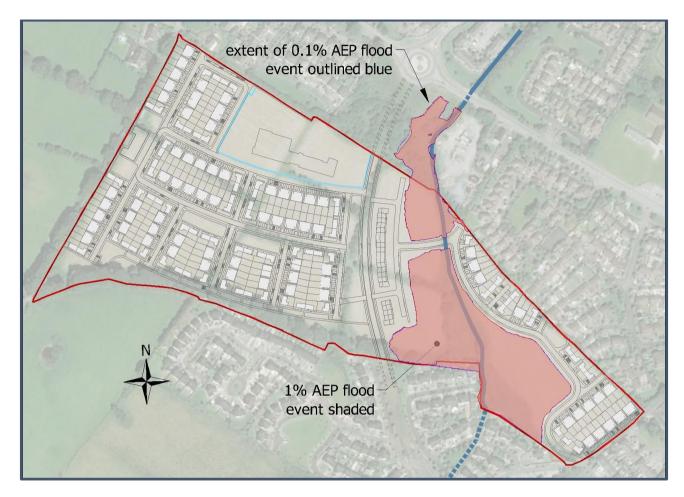
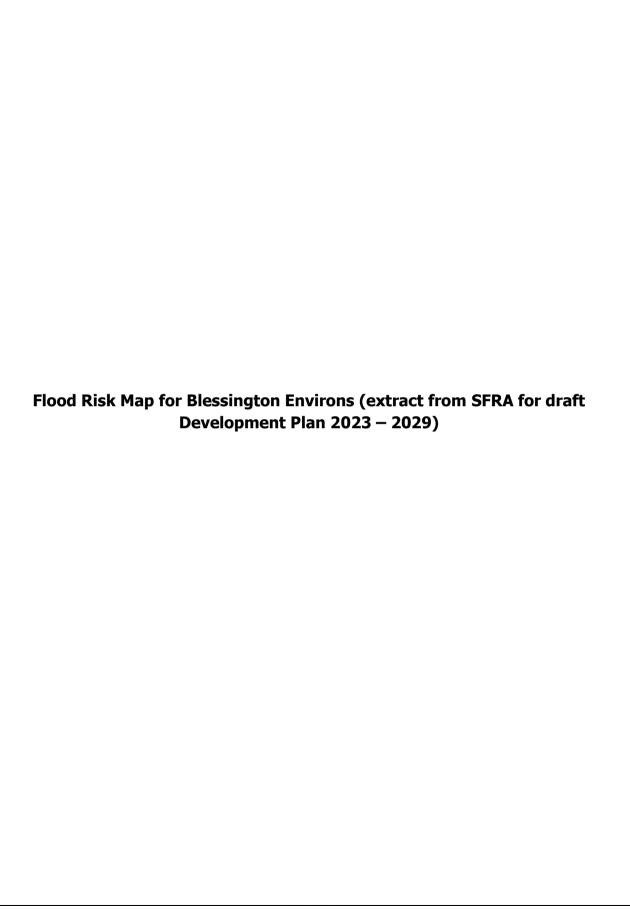


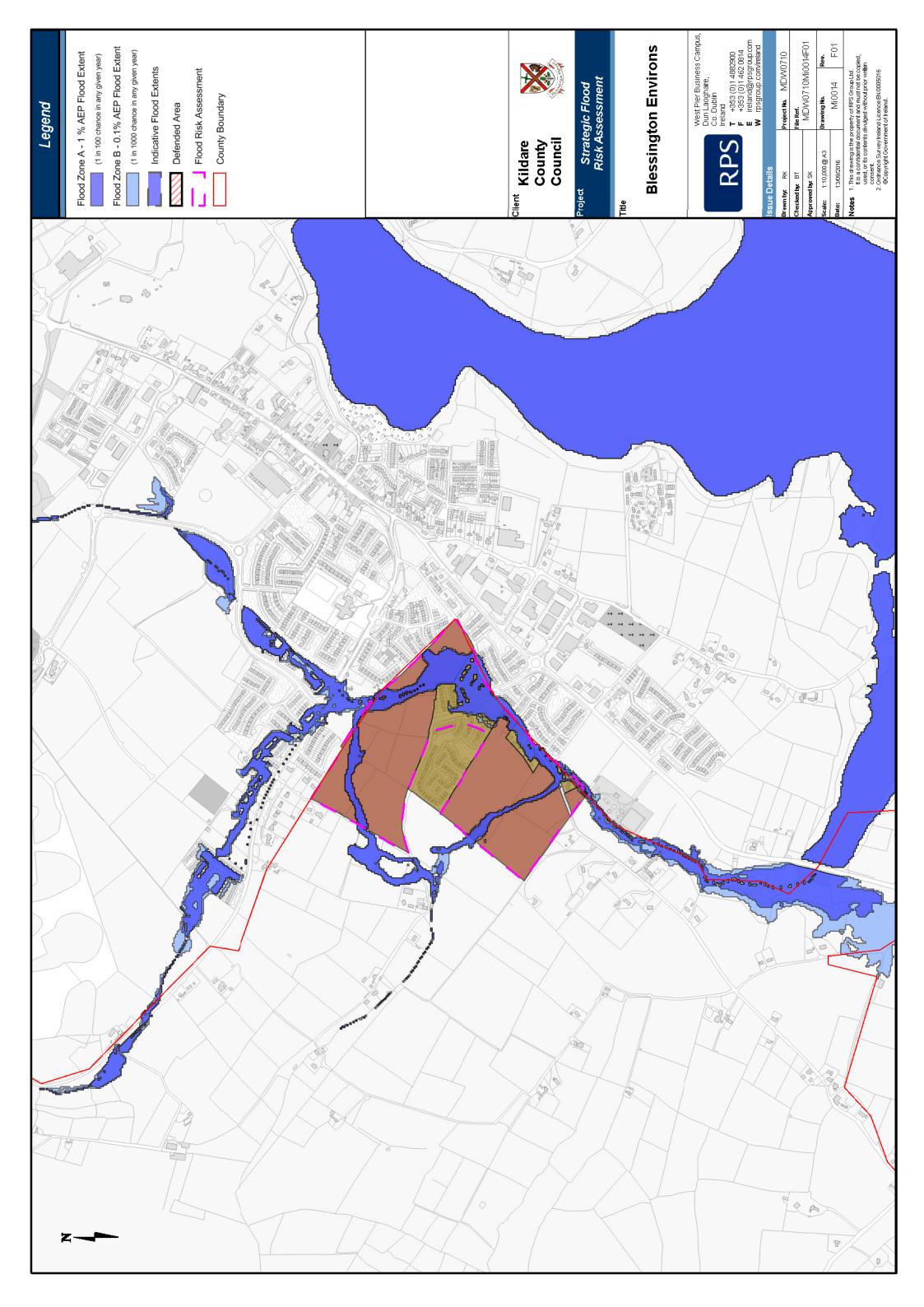
Figure 4-4 Flood Risk Zones Associated with Blessington Stream - Post-Development

4.6 Conclusion

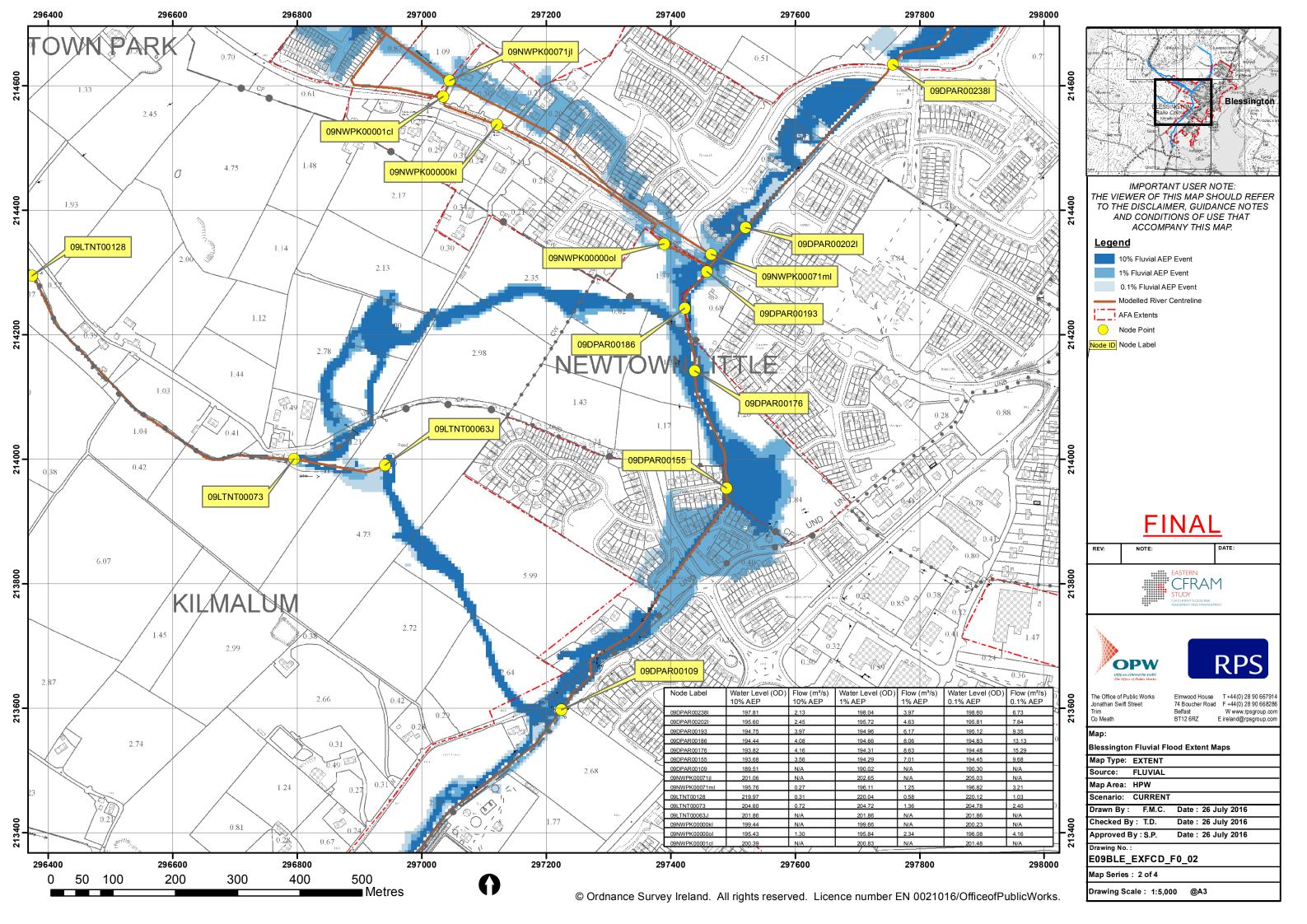
The detailed assessment demonstrates that development of the eastern part of the Site is possible while achieving full compliance with the Flood Risk Management Guidelines.

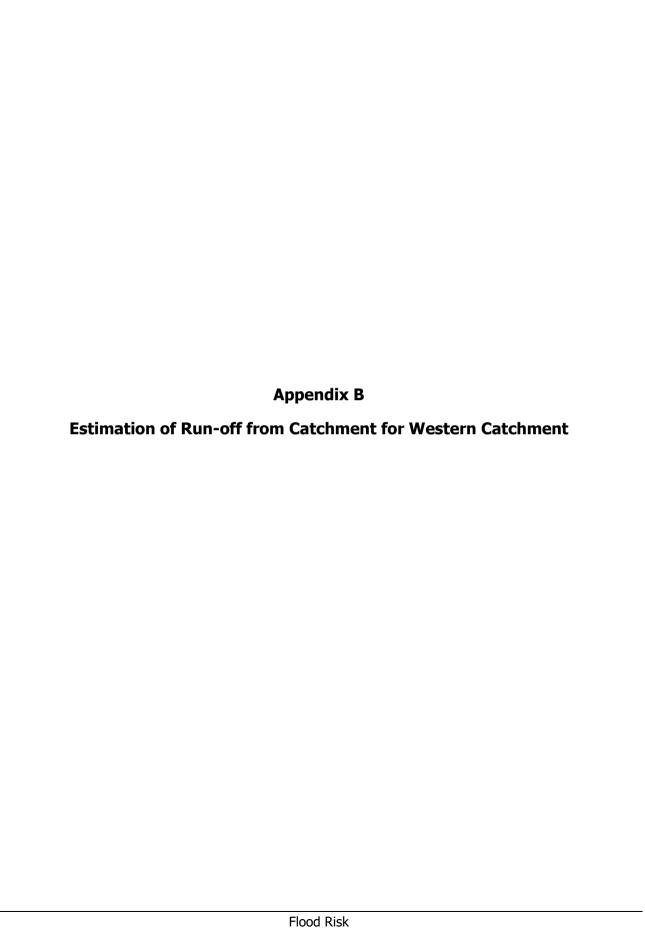




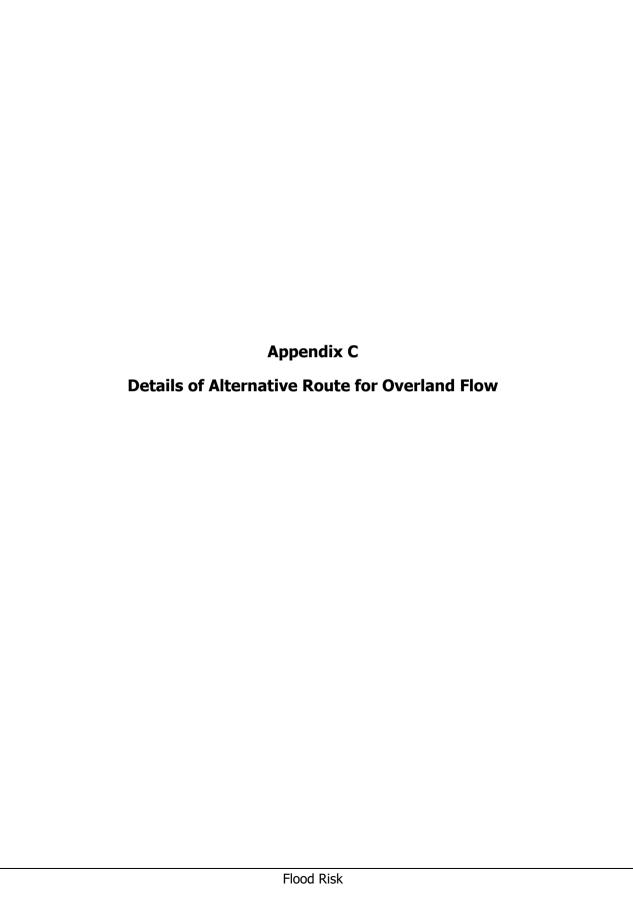


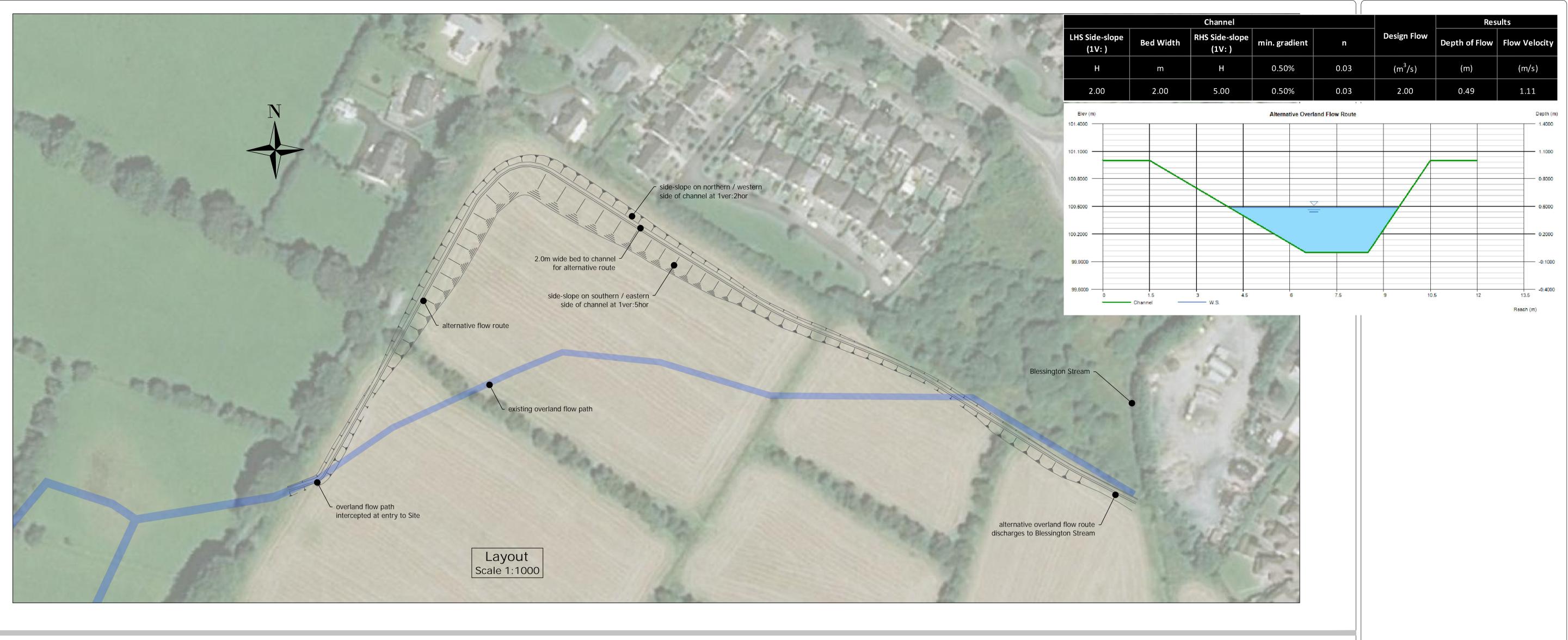


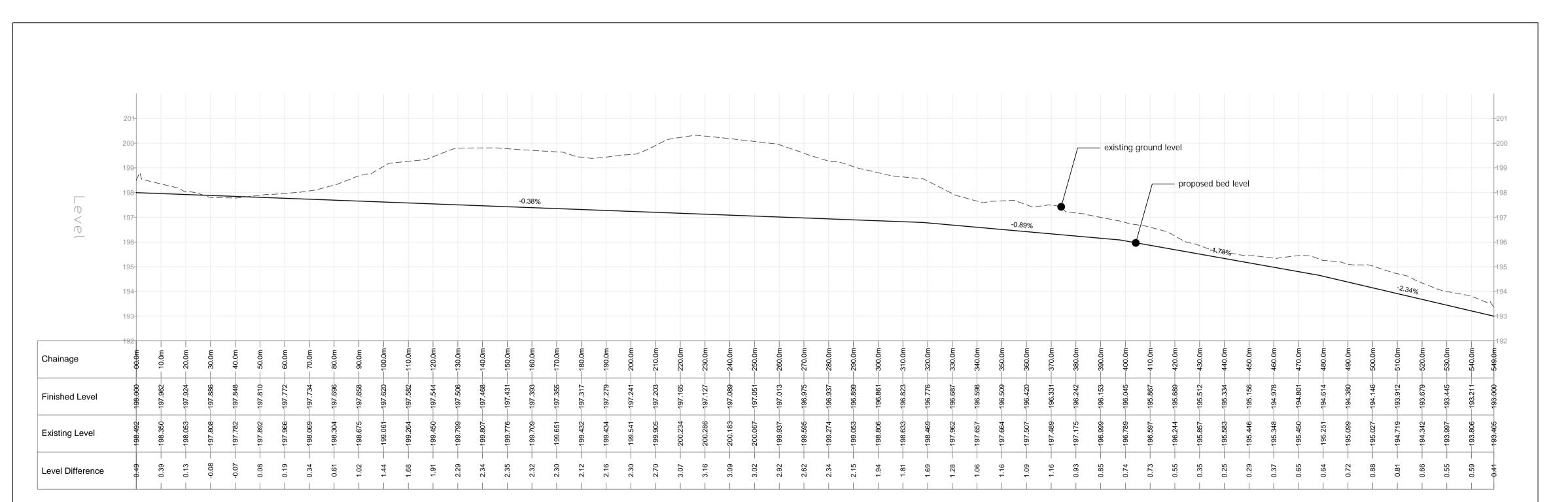




Estimation of Q $_{100}$ For Blessington SSFRA - IH124				
Characteristic	Value	Unit	Source	
Area (A)	0.8	km ²	FSU	
Average Annual Rainfall (SAAR)	966	mm		
G1 % =	0	%	Fig I 4.18	
G2 % =	100	%	Fig I 4.18	
G3 % =	0	%	Fig I 4.18	
G4 % =	0	%	Fig I 4.18	
G5 % =	0	%	Fig I 4.18	
Soil index (G) =	0.30	%		
Q _{BAR RURAL} =	0.19	m3/sec		
CWI =	123		Fig I 6.62	
CIND =	30.16		Eqn 7.2	
NC =	0.69		Eqn 7.3	
URBAN =	20.0	%		
Q BAR URBAN / Q BAR RURAL =	1.387		Eqn 7.4	
Q _{BAR} =	0.268	m3/sec		
Q ₁₀₀ / Q _{BAR} (Ireland)	1.96		FSR - Ireland	
Q _{1,000} / Q _{BAR} (Ireland)	2.6		FSR - Ireland	
Q ₁₀₀ =	0.524	m3/sec		
Q _{1,000} =	0.696	m3/sec		
Factorial Error Factor =	1.651		Page 37 IOH124	
Climate Change Factor =	1.2		GDSDS	
Q ₁₀₀ =	1.04	m3/sec	_ <u> </u> :	
Q _{1,000} =	1.38	m3/sec	2	

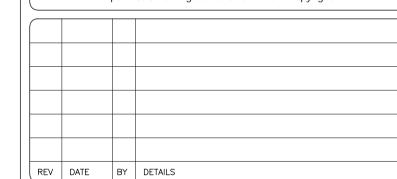






Profile Through Channel for Alternative Overland Flow Route Scale H 1:1000 V 1:100 OS mapping reproduced under licence.

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ZONING SUBMISSION FOR LANDS AT NEWTOWN LITTLE & NEWTOWNPARK, BLESSINGTON, CO. KILDARE

Alternative Overland Flow Route

SCALE:

as shown @ A1



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DRAWING NO.:
20003-OFR-01

REV.:
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SIZE: DATE: A1 23/05/22



Estimation of Q $_{100}$ For Blessington SSFRA - IH124				
Characteristic	Value	Unit	Source	
Area (A)	6.5	km²	FSU	
Average Annual Rainfall (SAAR)	966	mm		
G1 % =	0	%	Fig I 4.18	
G2 % =	100	%	Fig I 4.18	
G3 % =	0	%	Fig I 4.18	
G4 % =	0	%	Fig I 4.18	
G5 % =	0	%	Fig I 4.18	
Soil index (G) =	0.30	%		
Q BAR RURAL =	1.30	m3/sec		
CWI =	123		Fig I 6.62	
CIND =	30.16		Eqn 7.2	
NC =	0.69		Eqn 7.3	
URBAN =	20.0	%		
Q BAR URBAN / Q BAR RURAL =	1.387		Eqn 7.4	
Q _{BAR} =	1.801	m3/sec		
Q ₁₀₀ / Q _{BAR} (Ireland)	1.96		FSR - Ireland	
Q _{1,000} / Q _{BAR} (Ireland)	2.6		FSR - Ireland	
Q ₁₀₀ =	3.529	m3/sec		
Q _{1,000} =	4.682	m3/sec		
Factorial Error Factor =	1.651		Page 37 IOH124	
Climate Change Factor =	1.2		GDSDS	
Q ₁₀₀ =	6.99	m3/sec	 C	
Q _{1,000} =	9.28	m3/sec	c	